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# Negative group delay active topologies respectively dedicated to microwave frequencies and baseband signals

Blaise Ravelo, André Pérennec, Marc Le Roy

**Abstract** – This paper proposes and describes in details the synthesis, design and implementation of two different active topologies exhibiting negative group delay (NGD) in different frequency bands. With the first of them, gain and NGD in microwave frequency band are simultaneously achieved; the basic cell consists in a field effect transistor (FET) cascaded with a shunt RLC series network. The second topology brings also gain and NGD but is particularly dedicated to baseband signals; this circuit is also built with a FET; but this time in feedback with an RL series network. For both approaches, analytical formulas demonstrating the existence of gain and NGD are proposed together with details about the associated equations, at first for a single cell and then for multi-stage circuits. After implementation of each topology in a two-stage configuration, the results from experiments in frequency-domain are carefully compared to those from simulations; the same thing is done in time-domain for the baseband-dedicated device. Time-domain simulations and measurements highlight the high capability of both topologies to compensate or control various dispersive effects. Indeed for both circuits, in case of Gaussian-pulse or -modulated signal, the maximum of the output signal exhibits a time advance compared to the input one of respectively more than 40% and 60% of the standard deviation of the input signal. Moreover, this high relative time-advance is obtained with gain and a pulse compression phenomenon.

**Index terms** – Active circuits, negative group delay (NGD), time-domain, baseband signals, pulse compression.

## I. Introduction

Artificially constructed materials with simultaneously negative permittivity and permeability, also called “left-handed metamaterials” (LHM), have generated a growing interest in the scientific community. Among their properties not found in nature, the negative refractive index, the negative group velocity (NGV) and superluminal group velocity (faster than the speed of light in vacuum  $c$ ) that occur in LHM, have been particularly studied, discussed and experimentally observed in many configurations [1]-[5]. Of course, these abnormal velocities do not violate the requirements of relativistic causality. In the case of artificial lines with resonant cells that exhibit NGV in narrow frequency band [5], the output signal envelop is fully inscribed with the input one and the pulse advance can be explained through pulse reshaping. In region of anomalous dispersion, NGV is always associated with high transmission losses and is mainly narrowband.

Over the same time period, many authors [6]-[8] have, in parallel, proposed electronic circuits able to produce negative group delay (NGD) and mainly aimed at facilitating the observation of this phenomenon with classical test instruments contrarily to optical or quantum experiments [9]-[10]. These circuits being built with operational amplifier and localised components are, thus, restricted to low frequency because of the component bandwidth. They can produce both NGD and amplification for baseband signal up to a few kHz. Group velocity and group delay are related by the length of the device. Then, considering group delay is more convenient in the case of a circuit based on lumped components where the length is negligible compared to the wavelength. The group delay defines the time delay applied by the device on the wave packet envelop (or pulse for baseband signals).

The lack of devices with such characteristics, i.e. NGD and gain, in the domain of microwave frequencies, has led us to propose in [11]-[12] a new topology of NGD active circuit composed of a resonant RLC series network in cascade with a FET. We fully describe in this paper, the conditions to satisfy NGD, gain and active device requirements, the synthesis equations to design a single cell, and then a multi-stage circuit. With this topology, and contrarily to previous studies with passive or active implementations, NGD, gain and stability can be achieved over broad bands in the microwave domain. For a two-stage circuit, frequency simulations and measurements are compared, and used to generate time-domain simulations. In spite of promising abilities, this topology is intrinsically unable to provide NGD at very low frequencies. So, we propose here a new topology consisting in a FET feedbacked by an RL series network. This topology is used to produce gain and NGD from DC to hundreds of MHz and is then particularly devoted to baseband signals. An analytical investigation

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of these circuit characteristics is proposed and conditions to achieve our objectives are also extracted. Frequency- and time-domain experimental results are compared to simulations to validate our approach. Finally, conclusions are drawn concerning potential applications and limitations for each topology.

## II. Microwave NGD active topology

As stated in the previous section, the group delay,  $\tau_g$ , is the temporal shift of the wave packet through a device of length,  $L$ ; and this group delay is related to the group velocity,  $v_g$ , by:

$$(1) \quad \tau_g = \frac{d(kL)}{d\omega} = \frac{dk}{d\omega} L = \frac{L}{v_g}$$

where  $k$  is the  $\omega$ -dependent wave number. In the case of lumped-element circuit, where  $L$  is undefined or negligible compared to the wavelength, it is worth using the concept of group delay instead of group velocity. Indeed, when the scattering parameters are used, as done here, the group delay,  $\tau_g$ , is given by:

$$(2) \quad \tau_g = -\frac{d\phi(\omega)}{d\omega}$$

where  $\phi$  is the frequency-dependent transmission phase.

As, all the circuits or lines able to produce NGD at microwave frequencies were affected by high losses, our proposal was to start our study on NGD active circuit with a FET. The target topology had to meet the criteria of compromise between gain and NGD, stability, output/input matching while being rather simple.

At first, to get analytical expressions, we modelled the FET by a voltage-controlled current source of transconductance,  $g_m$ , in cascade with the drain-source resistor,  $R_{ds}$  (Figure1).

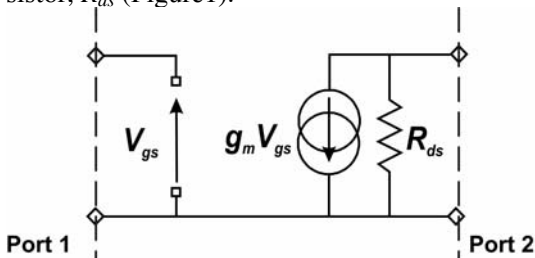


Fig. 1. FET modeling.

### A) Synthesis equations for a single NGD active cell

The presented NGD active topology devoted to microwave signals is based on a FET cascaded with a shunt series RLC resonant network as depicted in Fig-

ure 2. At the resonance frequency  $\omega_0 = 1/\sqrt{LC}$ , and for input and output reference ports normalized to  $Z_0$  ( $50 \Omega$  in practice), the transmission and output reflection parameters are defined as:

$$(3) \quad S_{21}(\omega_0) = \frac{-2RZ_0g_mR_{ds}}{R_{ds}R + Z_0(R + R_{ds})}$$

$$(4) \quad S_{22}(\omega_0) = \frac{R_{ds}R - Z_0(R + R_{ds})}{R_{ds}R + Z_0(R + R_{ds})}$$

At  $\omega_0$ ,  $S_{21}$  is minimum, but for any judicious values of  $R$ , its modulus can be greater than one and the output matching satisfied (less than -10 dB). Obtained from eq. (2), where  $\phi$  is the phase of the  $S_{21}$  parameter, the following expression (5) explicitly shows that the group delay is always negative:

$$(5) \quad \tau(\omega_0) = \frac{-2LZ_0R_{ds}}{R[R_{ds} + Z_0(R + R_{ds})]}$$

To get a significant NGD value,  $R$  must be small, but this is at the expense of the gain value. A satisfying compromise between gain and NGD is reached by setting  $L$  at a quite high value  $L$  and choosing a FET with high  $R_{ds}$  and  $g_m$  values.

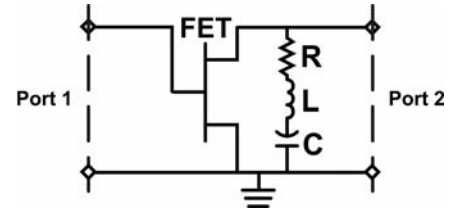


Fig. 2. First NGD active topology: FET in cascade with a shunt series resonant RLC network.

For a given transistor, synthesis equations are extracted from relations (3) to (5) in order to calculate the passive element values. These equations are given at the resonance frequency,  $\omega_0$ , and depend on the modulus of the transmission parameter,  $S_{21} = |S_{21}(\omega_0)|$ , the output return loss,  $S_{22} = |S_{22}(\omega_0)|$  and the NGD level,  $\tau = \tau(\omega_0)$ :

$$(6) \quad R = \frac{S_{21}R_{ds}Z_0}{2g_mZ_0R_{ds} - (R_{ds} + Z_0)S_{21}}$$

$$(7) \quad L = -\frac{\tau S_{21}g_m(R_{ds}Z_0)^2}{[2g_mR_{ds}Z_0 - (R_{ds} + Z_0)S_{21}]^2}$$

and  $C$  is simply deduced from the resonance frequency:

$$(8) \quad C = \frac{1}{L\omega_0^2}$$

It comes that the maximum reachable gain for this cell is defined in modulus by:

$$(9) \quad S_{21max}(\omega_0) = \frac{2g_m Z_0 R_{ds}}{Z_0 + R_{ds}}$$

One should note that this topology is that of a resistive amplifier, excepted for the components' values; indeed, contrary to resistive amplifier, the operating frequency is that of the resonant circuit.

### B) Design, simulation and experimental results of a two-stage microwave NGD active circuit

As we used in a first time a simplified FET modelling, we built in microstrip technology a two stage circuit aimed to operate at about 1 GHz to validate this approach. A schematic of an  $n$ -stage device is proposed in Figure 3. The input of the unit cell presented in Figure 2 is, of course, unmatched. So, the input matching of the first stage is ensured by the shunt resistor,  $R_m$ , calculated as:

$$(10) \quad R_m = Z_0 \frac{1 + S_{11}}{1 - S_{11}}$$

where  $S_{11}$  is the modulus of the desired input return loss of the first cell. On condition to consider that the first cell is as illustrated in Figure 3, the first stage resistor,  $R_1$ , is then expressed as a function of  $S_{11}$  and  $S_{22}$ :

$$(11) \quad R_1 = \frac{Z_0 R_{ds} S_{21}}{g_m Z_0 R_{ds} (1 + S_{11}) - S_{21} (Z_0 + R_{ds})}$$

Under this condition, the maximum insertion loss is modified as follows:

$$(12) \quad S_{21max} = \frac{g_m Z_0 R_{ds} (1 + S_{11})}{Z_0 + R_{ds}}$$

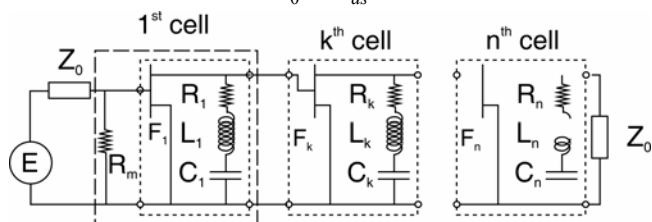


Fig. 3. Structure of the ideal  $n$ -stage circuit.

For an intermediate cell,  $k$ , the synthesis equations remain those previously described in eqs. (6)-(8). But,

for the  $n^{\text{th}}$  and last cell, eq. (6) is modified and expressed as a function of  $S_{22}$  of the last stage to match the circuit output:

$$(13) \quad R_n = \frac{(1 + S_{22}) R_{ds} Z_0}{R_{ds} - Z_0 - (R_{ds} + Z_0) S_{22}}$$

In order to get, at least, stability together with an input and output matching better than -10 dB, a NGD lower than -2 ns and loss compensation at least, we set both stages at the same resonance frequency. The first simulations using ADS microwave circuit simulator of Agilent<sup>TM</sup> showed that the adjustments to be made further to the introduction of connection lines and component spurious effects were very limited with respect to our first estimates. At last, we carried out an electromagnetic (EM) simulations and a slight optimisation.

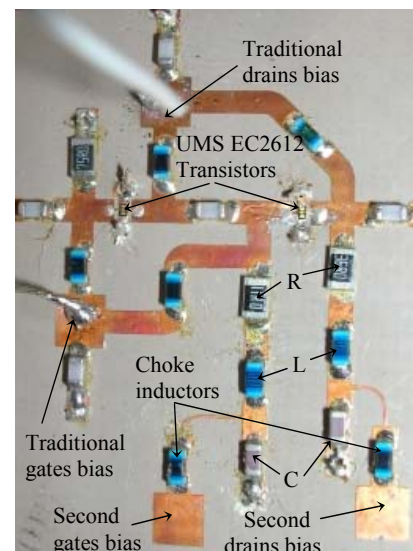
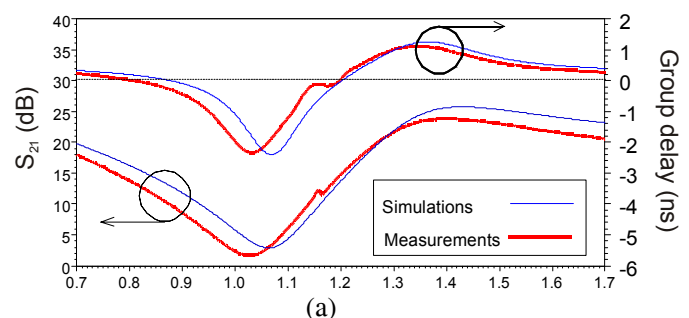
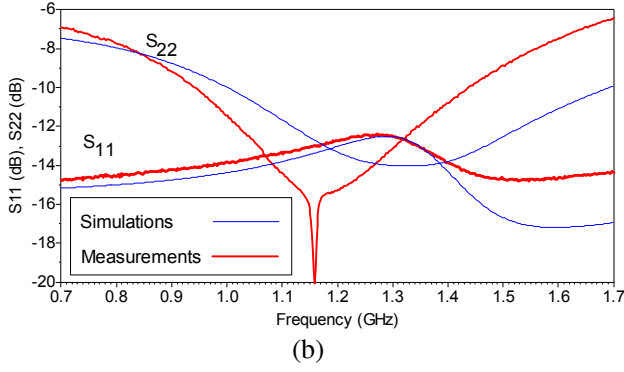


Fig. 4. Photograph of the two-stage active NGD device (28 mm  $\times$  22 mm). FET:  $g_m = 98.14$  mS and  $R_{ds} = 116.8 \Omega$ ,  $R_m = 75 \Omega$ ,  $R_1 = 11 \Omega$ ,  $R_2 = 36 \Omega$ ,  $L_1 = L_2 = 12$  nH,  $C_1 = C_2 = 1$  pF.

Figure 4 is a picture of the circuit layout with indications about the component characteristics.

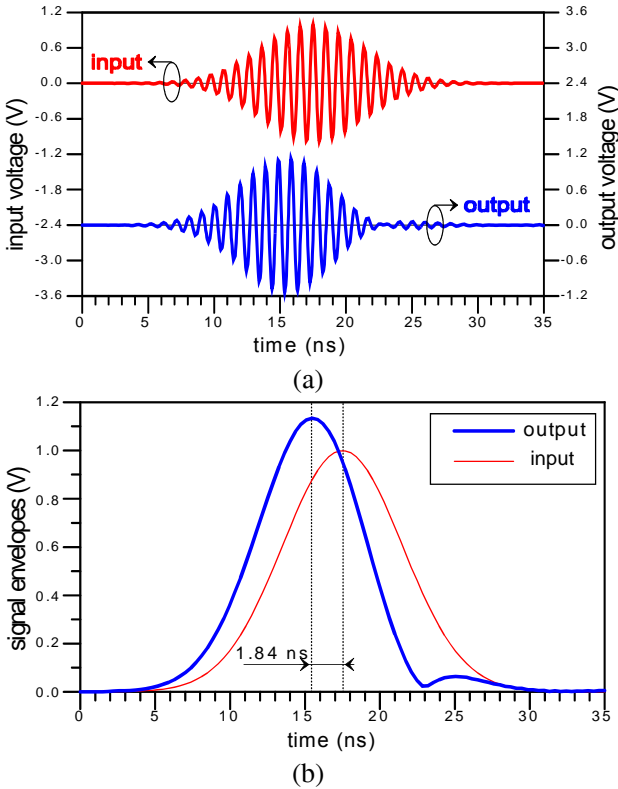


(a)



**Fig. 5.** (a) Measured  $S_{21}$  parameter and group delay and (b) output and input return losses.

To investigate for possible simplifications in the design of circuit bias networks, two different biasing paths were tested and gave similar results. In Figure 5, S-parameters and group delay measured by a vector network analyzer show a good agreement with electromagnetic simulation and confirm our expectations. It shows that, around 1 GHz, NGD is  $-2.3$  ns, gain is above 1 dB, input and output return losses are better than  $-10$  dB at the resonance and the overall circuit remains stable over the whole frequency band under measurement (up to 3 GHz). One should, however, note that the total group delay is not exactly the sum of individual cell group delays because of a slight inter-stage mismatch. The interest of having a device with NGD and gain is highlighted by time-domain results.



**Fig. 6.** Time responses simulated with the measured S-parameters (a) and the corresponding envelopes (b).

Those depicted in Figure 6 were extracted from the previous measured scattering parameters with an input signal consisting of a Gaussian pulse modulating a 1.03 GHz carrier. The output signal envelope shows an advance of about 46% of the time standard deviation (4 ns) of the input signal. One should note that, thanks to the gain and contrarily to previous studies with NGD microwave passive networks [4]-[5] or with electromagnetic bandgap [13], the output envelop is not fully inscribed in the input one. For the same number of cells as in [5], the time advance is equivalent, and the relative advance is higher because of the enlargement of the frequency bandwidth. A wide microwave frequency band with NGD and gain can be synthesised by applying different resonant frequencies to multi-stage circuits [14]. Finally, the main drawback of this topology is its natural inability to provide NGD at very low frequency, it therefore disqualifies it for baseband applications. Indeed, the following expression of the group delay at very low frequencies ( $\omega$  tends to zero) is always positive:

$$(14) \quad \tau(0) = \frac{CZ_0R_{ds}}{R_{ds} + Z_0}$$

As the first topology under study managed to fulfil our initial requirements; we propose a baseband topology around a FET, again.

### III. Baseband NGD active topology

We present the basic cell shown in fig 7 made of a FET feedbacked by an RL series network. Again, we use in a first approximation the FET modelling of Figure 1 and look for an interaction between the passive lumped components and the elements of this model.

#### A) Design equations

So, at a very low frequency ( $\omega$  tends to zero), the S-parameters of this cell are:

$$(15) \quad S_{11} = \frac{R_{ds}(R - Z_0^2 g_m) + Z_0(R - Z_0)}{R_{ds}(R + 2Z_0 + Z_0^2 g_m) + Z_0(R + Z_0)}$$

$$(16) \quad S_{12} = \frac{2Z_0 R_{ds}}{R_{ds}(R + 2Z_0 + Z_0^2 g_m) + Z_0(R + Z_0)}$$

$$(17) \quad S_{21} = \frac{2Z_0 R_{ds}(1 - g_m R)}{R_{ds}(R + 2Z_0 + Z_0^2 g_m) + Z_0(R + Z_0)}$$

$$(18) \quad S_{22} = \frac{R_{ds}(R - Z_0^2 g_m) - Z_0(R + Z_0)}{R_{ds}(R + 2Z_0 + Z_0^2 g_m) + Z_0(R + Z_0)}$$

From eqs. (15), (17) and (18), the input- and output-return losses can be expressed as a function of the insertion loss,  $|S_{21}|$  leading to:

$$(19) \quad S_{11} = \frac{R_{ds}(1 - Z_0 g_m) + |S_{21}|(Z_0 + R_{ds})}{R_{ds}(Z_0 g_m + 1)}$$

$$(20) \quad S_{22} = \frac{R_{ds}(1 + |S_{21}|) - Z_0(1 + g_m R_{ds})}{Z_0(1 + g_m R_{ds}) + R_{ds}}$$

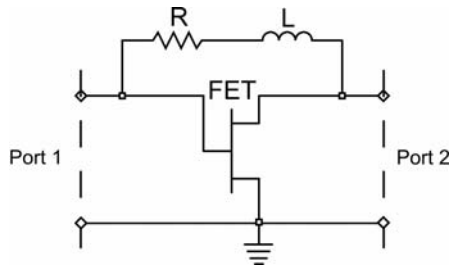


Fig. 7. Baseband NGD active cell.

Amplifier stability required a special care. So, for a given transistor, by using eqs. (19)-(20), and according to  $S_{21}$ , we define a region where, a priori, input and output matching is gotten. Figure 8 illustrates these conditions (for  $g_m$  and  $R_{ds}$  values of part II-B), where the hatched area is to be avoided.

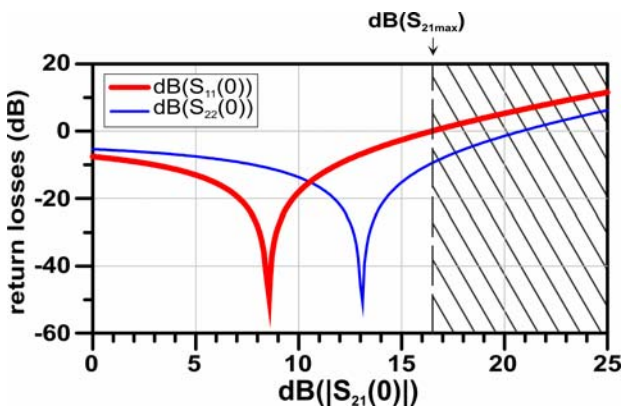


Fig. 8. Input and output return losses ( $dB(S_{11})$ ,  $dB(S_{22})$ ) versus gain ( $dB(S_{21})$ ).

To alleviate this problem of instability, resistors can be placed in series at the input and output accesses. For the basic cell of Figure 7, the group delay is given by:

$$(21) \quad \tau(0) = \frac{(1 + g_m Z_0)L[R_{ds} + Z_0(1 + g_m R_{ds})]}{(1 - g_m R)[R_{ds}(R + 2Z_0 + Z_0^2 g_m) + Z_0(R + Z_0)]}$$

which becomes negative when:

$$(22) \quad R > 1/g_m$$

Under such conditions, the NGD bandwidth goes from DC to the angular cut-off frequency,  $\omega_c$ , which is as follows:

$$(23) \quad \omega_c^2 = \frac{[2g_m Z_0 R_{ds} - |S_{21}(0)|(R_{ds} + Z_0)]^2}{2\tau^2(0)|S_{21}(0)|g_m Z_0 R_{ds}(R_{ds} + Z_0)}$$

As  $\omega_c$  is inversely proportional to  $|\tau(0)|$ , it implies to use a multi-stage circuit to get a significant broadband of gain and NGD.

Moreover, the signs of the output and input signals being unlike, the number of stages must be even. This is also true for the first topology under study; it appears as less problematic when the signals are modulated. Inversion of eqs. (15) and (20) gives the following synthesis relations for  $R$  and  $L$ :

$$(24) \quad R = \frac{Z_0[2R_{ds} + |S_{21}(0)|(Z_0 + 2R_{ds} + Z_0 g_m R_{ds})]}{2Z_0 g_m R_{ds} - |S_{21}(0)|(Z_0 + R_{ds})}$$

$$(25) \quad L = \frac{2\tau(0)Z_0 g_m R_{ds} |S_{21}(0)|(1 + Z_0 g_m)[R_{ds} + Z_0(1 + g_m R_{ds})]}{-[|S_{21}(0)|(Z_0 + R_{ds}) - 2Z_0 g_m R_{ds}]^2}$$

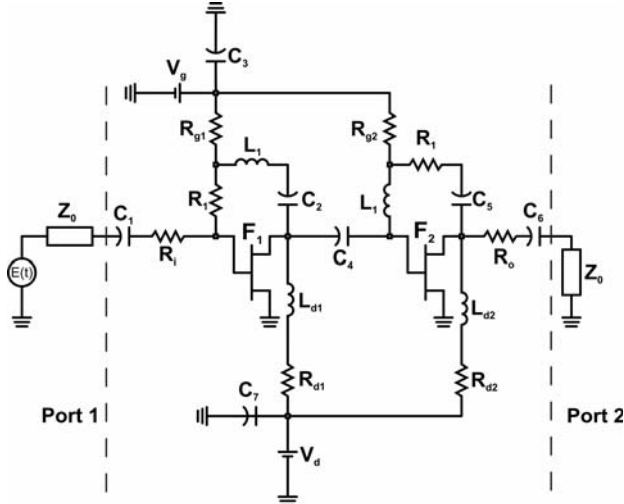
Both were used to determine the initial values of the cell components. It is worth noting that, for a given FET, a satisfying compromise between gain and NGD can be quickly found by plotting sets of parametric curves. The maximum gain is also given by eq. (9) and depends only on the reference impedance and transistor characteristics ( $g_m$ ,  $R_{ds}$ ).

## B) Implementation of a two-stage baseband NGD active circuit and frequency- and time-domain measurements

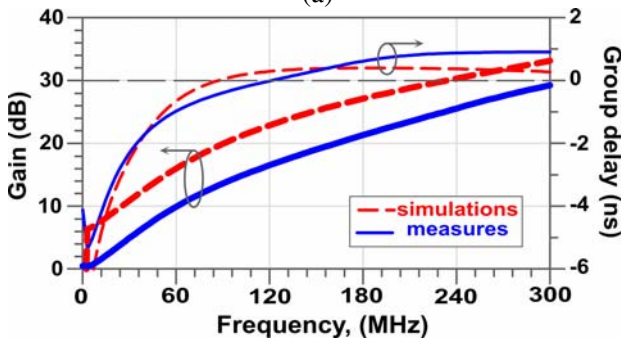
Figure 9 presents the schematic of the device under study, which consists of a two-stage circuit with input and output matching series resistors; it gives also the bias networks and the component values. Combined results of EM simulations of the printed circuit with circuit simulations of the localized components are compared to measurements in Figures 9-b and 9-c. The differences between simulations and measurements in Figures 9-a and 9-b are mainly due to extrapolation of the transistor S-parameters from the manufacturer datasheet in that frequency band. A satisfying agreement is nevertheless obtained for the NGD characteristics. The measured group delay is negative up to more than 100 MHz with simultaneous gain. A wider NGD bandwidth could be produced by applying this method with more stages. But, to easily perform a time domain validation, the number of components was voluntarily limited and the selected



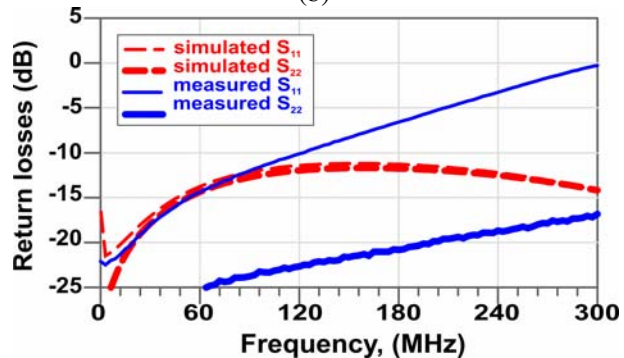
frequency band was compatible with test instruments available within our lab.



(a)



(b)



(c)

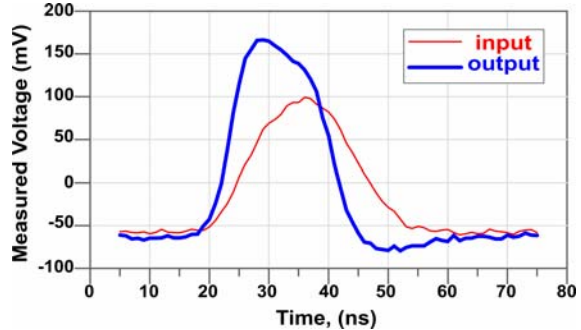
**Fig. 9.** -a) Schematic of the two-stage baseband NGD active circuit including biasing networks;  $R_1 = R_2 = 68\Omega$ ,  $R_i = R_o = 33\Omega$ ,  $L_1 = 270\text{nH}$ ,  $L_{d1} = L_{d2} = 1\mu\text{H}$ ,  $R_{d1} = R_{d2} = 68\Omega$ ,  $R_{g1} = R_{g2} = 1\text{k}\Omega$ ,  $C_{1-7} = 22\mu\text{F}$ , and  $F_1 = F_2 = \text{FET} = \text{ATF-55143}$  ( $g_m = 220\text{ mS}$ ,  $R_{ds} = 230\Omega$ )

-b) gain  $\text{dB}(S_{21})$  and group delay  $\tau_{21}$ .

-c) input and output return losses ( $\text{dB}(S_{11})$  and  $\text{dB}(S_{22})$ ).

The measurements were made by using a function generator delivering, in practice, a signal close to a Gaussian pulse (8 ns standard deviation) and a 2Gs/s LeCroy Digital oscilloscope. Input and output circuit accesses were directly connected to the scope through coaxial tee with no cable to avoid spurious reflections or delays. The cumulate delay (approximately 1 ns)

due to the input and output tees has been deembedded from initial measurements prior to the production of Figure 10 in order to place time- and frequency-domain measurements in the same reference planes (as defined by ports 1 and 2 in Figure 9-a).



**Fig. 10.** Time-domain experimental input and output curves for the NGD baseband circuit.

Finally, for a same ordinate scale, Figure 10 shows that the output pulse maximum has a time advance of more than 60% (more of 5 ns) with respect to the input standard deviation with a slight distortion.

## IV. Conclusion

We proposed two different ways to generate NGD without losses. The conditions required to get NGD, gain and the design requirements of active device were introduced from analytical relations. Each topology was scrupulously validated through the measurements of corresponding two-stage prototypes. The first topology, thanks to its simplicity, its possibility of achieving broad bandwidth, and loss compensation, could be applied to compensate dispersive effects or in the design of UWB phase shifters by using the area of positive phase slope. However, its intrinsic limitation at low frequency led us to investigate another topology more dedicated to baseband signals. The prototype proposed here meets this requirements and seems particularly well suited to find applications in interconnect delay compensation. Indeed, the group delay proved to be only negative up to a hundred of MHz for measurements convenience, but a wider bandwidth could be achieved by a device with more stages.

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